Axially Loaded Numbers

Changes in Lengths of Axially Loaded Members

Problem 2.2-1 The T-shaped arm ABC shown in the figure lies in a vertical plane and pivots about a horizontal pin at A. The arm has constant cross-sectional area and total weight W. A vertical spring of stiffness k supports the arm at point B.

2

Obtain a formula for the elongation δ of the spring due to the weight of the arm.

FREE-BODY DIAGRAM OF ARM $F = \text{tensile force in the spring}$

$$
\Sigma M_A = 0 \Leftrightarrow \Leftrightarrow
$$
\n
$$
F(b) - \frac{W}{3} \left(\frac{b}{2}\right) - \frac{W}{3} \left(\frac{3b}{2}\right) - \frac{W}{3} (2b) = 0
$$
\n
$$
F = \frac{4W}{3}
$$
\n
$$
\delta = \text{elongation of the spring}
$$
\n
$$
\delta = \frac{F}{k} = \frac{4W}{3k}
$$

b \longrightarrow *b*

AB C

k

Problem 2.2-2 A steel cable with nominal diameter 25 mm (see Table 2-1) is used in a construction yard to lift a bridge section weighing 38 kN, as shown in the figure. The cable has an effective modulus of elasticity $E = 140$ GPa.

- (a) If the cable is 14 m long, how much will it stretch when the load is picked up?
- (b) If the cable is rated for a maximum load of 70 kN, what is the factor of safety with respect to failure of the cable?

b

(b) FACTOR OF SAFETY
\n
$$
P_{ULT} = 406 \text{ kN (from Table 2-1)}
$$
\n
$$
P_{\text{max}} = 70 \text{ kN}
$$
\n
$$
n = \frac{P_{ULT}}{P_{\text{max}}} = \frac{406 \text{ kN}}{70 \text{ kN}} = 5.8 \leftarrow
$$

(a) STRETCH OF CABLE

$$
\delta = \frac{WL}{EA} = \frac{(38 \text{ kN})(14 \text{ m})}{(140 \text{ GPa})(304 \text{ mm}^2)}
$$

= 12.5 mm

Problem 2.2-3 A steel wire and a copper wire have equal lengths and support equal loads *P* (see figure). The moduli of elasticity for the steel and copper are $E_s = 30,000$ ksi and $E_c = 18,000$ ksi, respectively.

- (a) If the wires have the same diameters, what is the ratio of the elongation of the copper wire to the elongation of the steel wire?
- (b) If the wires stretch the same amount, what is the ratio of the diameter of the copper wire to the diameter of the steel wire?

Solution 2.2-3 Steel wire and copper wire

(b) RATIO OF DIAMETERS (EQUAL ELONGATIONS)

$$
\delta_c = \delta_s \quad \frac{PL}{E_c A_c} = \frac{PL}{E_s A_s} \text{ or } E_c A_c = E_s A_s
$$

$$
E_c \left(\frac{\pi}{4}\right) d_c^2 = E_s \left(\frac{\pi}{4}\right) d_s^2
$$

$$
\frac{d_c^2}{d_s^2} = \frac{E_s}{E_c} \quad \frac{d_c}{d_s} = \sqrt{\frac{E_s}{E_c}} = \sqrt{\frac{30}{18}} = 1.29 \quad \longleftarrow
$$

Problem 2.2-4 By what distance *h* does the cage shown in the figure move downward when the weight *W* is placed inside it?

Consider only the effects of the stretching of the cable, which has axial rigidity $EA = 10,700$ kN. The pulley at *A* has diameter d_A = 300 mm and the pulley at *B* has diameter d_B = 150 mm. Also, the distance $L_1 = 4.6$ m, the distance $L_2 = 10.5$ m, and the weight $W = 22$ kN. (*Note:* When calculating the length of the cable, include the parts of the cable that go around the pulleys at *A* and *B*.)

Solution 2.2-4 Cage supported by a cable

LENGTH OF CABLE $= 4,600$ mm $+ 21,000$ mm $+ 236$ mm $+ 236$ mm $= 26,072$ mm ELONGATION OF CABLE LOWERING OF THE CAGE $h =$ distance the cage moves downward $h = \frac{1}{2}\delta = 13.4$ mm $\delta = \frac{TL}{EA} = \frac{(11 \text{ kN})(26,072 \text{ mm})}{(10,700 \text{ kN})} = 26.8 \text{ mm}$ $L = L_1 + 2L_2 + \frac{1}{4}$ $\frac{1}{4}(\pi d_A) + \frac{1}{2}$ $\frac{1}{2}(\pi d_B)$

Problem 2.2-5 A safety valve on the top of a tank containing steam under pressure *p* has a discharge hole of diameter *d* (see figure). The valve is designed to release the steam when the pressure reaches the value p_{max} .

If the natural length of the spring is *L* and its stiffness is *k*, what should be the dimension *h* of the valve? (Express your result as a formula for *h.*)

Solution 2.2-5 Safety valve

- h = height of valve (compressed length of the spring)
- $d =$ diameter of discharge hole
- $P =$ pressure in tank

 p_{max} = pressure when valve opens

- $L =$ natural length of spring $(L > h)$
- $k =$ stiffness of spring

FORCE IN COMPRESSED SPRING

$$
F = k(L - h)
$$
 (From Eq. 2-1a)

PRESSURE FORCE ON SPRING

$$
P = p_{\text{max}} \left(\frac{\pi d^2}{4} \right)
$$

EQUATE FORCES AND SOLVE FOR *h*:

$$
F = P \quad k(L - h) = \frac{\pi p_{\text{max}} d^2}{4}
$$

$$
h = L - \frac{\pi p_{\text{max}} d^2}{4k} \quad \longleftarrow
$$

Problem 2.2-6 The device shown in the figure consists of a pointer *ABC* supported by a spring of stiffness $k = 800$ N/m. The spring is positioned at distance $b = 150$ mm from the pinned end *A* of the pointer. The device is adjusted so that when there is no load *P*, the pointer reads zero on the angular scale.

If the load $P = 8$ N, at what distance *x* should the load be placed so that the pointer will read 3° on the scale?

Solution 2.2-6 Pointer supported by a spring

 $\Sigma M_A = 0$ \curvearrowleft

$$
-Px + (k\delta)b = 0 \quad \text{or} \quad \delta = \frac{Px}{kb}
$$

Let α = angle of rotation of pointer

$$
\tan \alpha = \frac{\delta}{b} = \frac{Px}{kb^2} \quad x = \frac{kb^2}{P} \tan \alpha \ \ \Longleftrightarrow
$$

SUBSTITUTE NUMERICAL VALUES:

$$
\alpha = 3^{\circ}
$$

$$
x = \frac{(800 \text{ N/m})(150 \text{ mm})^2}{8 \text{ N}} \tan 3^{\circ}
$$

= 118 mm

b

A

C

P

b

b

B

D

Problem 2.2-7 Two rigid bars, *AB* and *CD*, rest on a smooth horizontal surface (see figure). Bar *AB* is pivoted end *A* and bar *CD* is pivoted at end *D*. The bars are connected to each other by two linearly elastic springs of stiffness *k*. Before the load *P* is applied, the lengths of the springs are such that the bars are parallel and the springs are without stress.

Derive a formula for the displacement δ_c at point *C* when the load *P* is acting. (Assume that the bars rotate through very small angles under the action of the load *P*.)

Solution 2.2-7 Two bars connected by springs

 $k =$ stiffness of springs

 δ_C = displacement at point *C* due to load *P*

FREE-BODY DIAGRAMS

 F_1 = tensile force in first spring F_2 = compressive force in second spring

EQUILIBRIUM -

$$
\Sigma M_A = 0 \t -bF_1 + 2bF_2 = 0 \t F_1 = 2F_2
$$

\n
$$
\Sigma M_D = 0 \t 2bP - 2bF_1 + bF_2 = 0 \t F_2 = 2F_1 - 2P
$$

\nSolving, $F_1 = \frac{4P}{3}$ $F_2 = \frac{2P}{3}$

DISPLACEMENT DIAGRAMS

 δ_B = displacement of point *B*

 δ_C = displacement of point *C*

 Δ_1 = elongation of first spring

$$
= \delta_C - \frac{\delta_B}{2}
$$

 Δ_2 = shortening of second spring

$$
= \delta_B - \frac{c_C}{2}
$$

Also,
$$
\Delta_1 = \frac{F_1}{k} = \frac{4P}{3k}; \quad \Delta_2 = \frac{F_2}{k} = \frac{2P}{3k}
$$

SOLVE THE EQUATIONS:

^C

$$
\Delta_1 = \Delta_1 \quad \delta_C - \frac{\delta_B}{2} = \frac{4P}{3k}
$$

$$
\Delta_2 = \Delta_2 \quad \delta_B - \frac{\delta_C}{2} = \frac{2P}{3k}
$$

Eliminate δ_B and obtain δ_C :

$$
\delta_C = \frac{20P}{9k} \leftarrow
$$

Problem 2.2-8 The three-bar truss *ABC* shown in the figure has a span $L = 3$ m and is constructed of steel pipes having cross-sectional area $A = 3900$ mm² and modulus of elasticity $E = 200$ GPa. A load *P* acts horizontally to the right at joint *C*.

- (a) If $P = 650$ kN, what is the horizontal displacement of joint *B*?
- (b) What is the maximum permissible load P_{max} if the displacement of joint *B* is limited to 1.5 mm?

Solution 2.2-8 Truss with horizontal load

 $L = 3$ m

 $A = 3900$ mm²

 $E = 200$ GPa

$$
\Sigma M_A = 0
$$
 gives $R_B = \frac{P}{2}$

FREE-BODY DIAGRAM OF JOINT *B*

Force triangle:

From force triangle,

$$
F_{AB} = \frac{P}{2}
$$
 (tension)

(a) HORIZONTAL DISPLACEMENT δ_B

$$
P = 650 \text{ kN}
$$

$$
\delta_B = \frac{F_{AB} L_{AB}}{EA} = \frac{PL}{2EA}
$$

=
$$
\frac{(650 \text{ kN})(3 \text{ m})}{2(200 \text{ GPa})(3900 \text{ mm}^2)}
$$

= 1.25 mm

(b) MAXIMUM LOAD P_{max}

$$
\delta_{\text{max}} = 1.5 \text{ mm}
$$

$$
\frac{P_{\text{max}}}{\delta_{\text{max}}} = \frac{P}{\delta} \qquad P_{\text{max}} = P\left(\frac{\delta_{\text{max}}}{\delta}\right)
$$

$$
P_{\text{max}} = (650 \text{ kN}) \left(\frac{1.5 \text{ mm}}{1.25 \text{ mm}}\right)
$$

= 780 kN

Problem 2.2-9 An aluminum wire having a diameter $d = 2$ mm and length $L = 3.8$ m is subjected to a tensile load *P* (see figure). The aluminum has modulus of elasticity $E = 75$ GPa.

If the maximum permissible elongation of the wire is 3.0 mm and the allowable stress in tension is 60 MPa, what is the allowable load P_{max} ?

Solution 2.2-9 Aluminum wire in tension

$$
\delta_{\text{max}} = 3.0 \text{ mm} \quad \delta = \frac{PL}{EA}
$$

$$
\frac{1}{2}
$$

Elongation governs. $P_{\text{max}} = 186 \text{ N} \longleftarrow$

Problem 2.2-10 A uniform bar *AB* of weight $W = 25$ N is supported by two springs, as shown in the figure. The spring on the left has stiffness $k_1 = 300$ N/m and natural length $L_1 = 250$ mm. The corresponding quantities for the spring on the right are $k₂ = 400$ N/m and $L_2 = 200$ mm. The distance between the springs is $L = 350$ mm, and the spring on the right is suspended from a support that is distance $h = 80$ mm below the point of support for the spring on the left.

At what distance *x* from the left-hand spring should a load $P = 18$ N be placed in order to bring the bar to a horizontal position?

Solution 2.2-10 Bar supported by two springs

Reference line

- $k_2 = 400$ N/m
- $L = 350$ mm
- $h = 80$ mm
- $P = 18 N$

NATURAL LENGTHS OF SPRINGS

 $L_1 = 250$ mm $L_2 = 200$ mm

OBJECTIVE

Find distance *x* for bar *AB* to be horizontal.

FREE-BODY DIAGRAM OF BAR *AB*

$$
\Sigma M_A = 0 \Leftrightarrow \Leftrightarrow
$$

F₂L - P_X - $\frac{WL}{2}$ = 0 \t\t (Eq. 1)

$$
\Sigma F_{\text{vert}} = 0 \quad \uparrow_{+} \quad \downarrow^{-}
$$

$$
F_1 + F_2 - P - W = 0
$$
 (Eq. 2)

SOLVE EQS. (1) AND (2):

$$
F_1 = P\left(1 - \frac{x}{L}\right) + \frac{W}{2}
$$
 $F_2 = \frac{P_X}{L} + \frac{W}{2}$

SUBSTITUTE NUMERICAL VALUES:

UNITS: Newtons and meters

$$
F_1 = (18)\left(1 - \frac{x}{0.350}\right) + 12.5 = 30.5 - 51.429x
$$

$$
F_2 = (18)\left(\frac{x}{0.350}\right) + 12.5 = 51.429x + 12.5
$$

ELONGATIONS OF THE SPRINGS

$$
\delta_1 = \frac{F_1}{k_1} = \frac{F_1}{300} = 0.10167 - 0.17143x
$$

$$
\delta_2 = \frac{F_2}{k_2} = \frac{F_2}{400} = 0.12857x + 0.031250
$$

BAR *AB* REMAINS HORIZONTAL

Points *A* and *B* are the same distance below the reference line (see figure above).

$$
\therefore L_1 + \delta_1 = h + L_2 + \delta_2
$$

or 0.250 + 0.10167 - 0.17143 x
= 0.080 + 0.200 + 0.12857 x + 0.031250

SOLVE FOR *x*:

 $0.300 x = 0.040420$ $x = 0.1347$ m

 $x = 135$ mm \leftarrow

Problem 2.2-11 A hollow, circular, steel column $(E = 30,000 \text{ ksi})$ is subjected to a compressive load P , as shown in the figure. The column has length $L = 8.0$ ft and outside diameter $d = 7.5$ in. The load $P = 85$ k.

If the allowable compressive stress is 7000 psi and the allowable shortening of the column is 0.02 in., what is the minimum required wall thickness t_{\min} ?

Solution 2.2-11 Column in compression

 $P = 85 k$

 $E = 30,000$ ksi

 $L = 8.0$ ft

 $d = 7.5$ in.

 $\sigma_{\rm allow}$ = 7,000 psi $\delta_{\rm allow} = 0.02$ in.

REQUIRED AREA BASED UPON ALLOWABLE STRESS

$$
\sigma = \frac{P}{A} \quad A = \frac{P}{\sigma_{\text{allow}}} = \frac{85 \text{ k}}{7,000 \text{ psi}} = 12.14 \text{ in.}^2
$$

REQUIRED AREA BASED UPON ALLOWABLE SHORTENING

$$
\delta = \frac{PL}{EA} \quad A = \frac{PL}{E\delta_{\text{allow}}} = \frac{(85 \text{ k})(96 \text{ in.})}{(30,000 \text{ ksi})(0.02 \text{ in.})}
$$

= 13.60 in.²
ShORTENING GOVERNS
 $A_{\text{min}} = 13.60 \text{ in.}^2$
MINIMUM THICKNESS t_{min}

$$
A = \frac{\pi}{4} [d^2 - (d - 2t)^2] \quad \text{or} \quad \frac{4A}{\pi} - d^2
$$

$$
= -(d - 2t)^2
$$

$$
(d - 2t)^2 = d^2 - \frac{4A}{\pi} \quad \text{or} \quad d - 2t = \sqrt{d^2 - \frac{4A}{\pi}}
$$

$$
t = \frac{d}{2} - \sqrt{\left(\frac{d}{2}\right)^2 - \frac{A}{\pi}} \quad \text{or}
$$

$$
t_{\text{min}} = \frac{d}{2} - \sqrt{\left(\frac{d}{2}\right)^2 - \frac{A_{\text{min}}}{\pi}}
$$

SUBSTITUTE NUMERICAL VALUES

$$
t_{\min} = \frac{7.5 \text{ in.}}{2} - \sqrt{\left(\frac{7.5 \text{ in.}}{2}\right)^2 - \frac{13.60 \text{ in.}^2}{\pi}}
$$

$$
t_{\min} = 0.63 \text{ in.} \longleftarrow
$$

Problem 2.2-12 The horizontal rigid beam *ABCD* is supported by vertical bars *BE* and *CF* and is loaded by vertical forces $P_1 = 400$ kN and $P_2 = 360$ kN acting at points *A* and *D*, respectively (see figure). Bars *BE* and *CF* are made of steel $(E = 200 \text{ GPa})$ and have cross-sectional areas A_{BE} = 11,100 mm² and A_{CF} = 9,280 mm². The distances between various points on the bars are shown in the figure.

Determine the vertical displacements δ_A and δ_D of points *A* and *D*, respectively.

Solution 2.2-12 Rigid beam supported by vertical bars

 $(400 \text{ kN})(3.0 \text{ m}) - F_{BE}(1.5 \text{ m}) - (360 \text{ kN})(2.1 \text{ m}) = 0$ F_{BE} = 296 kN $\sum M_C = 0$ \curvearrowleft

SHORTENING OF BAR *BE*

$$
\delta_{BE} = \frac{F_{BE} L_{BE}}{EA_{BE}} = \frac{(296 \text{ kN})(3.0 \text{ m})}{(200 \text{ GPa})(11,100 \text{ mm}^2)}
$$

$$
= 0.400 \text{ mm}
$$

SHORTENING OF BAR *CF*

$$
\delta_{CF} = \frac{F_{CF} L_{CF}}{EA_{CF}} = \frac{(464 \text{ kN})(2.4 \text{ m})}{(200 \text{ GPa})(9,280 \text{ mm}^2)}
$$

$$
= 0.600 \text{ mm}
$$

DISPLACEMENT DIAGRAM

$$
\delta_{BE} - \delta_A = \delta_{CF} - \delta_{BE} \quad \text{or} \quad \delta_A = 2\delta_{BE} - \delta_{CF}
$$

\n
$$
\delta_A = 2(0.400 \text{ mm}) - 0.600 \text{ m}
$$

\n= 0.200 mm
\n(Downward)
\n
$$
\delta_D - \delta_{CF} = \frac{2.1}{1.5} (\delta_{CF} - \delta_{BE})
$$

\nor
$$
\delta_D = \frac{12}{5} \delta_{CF} - \frac{7}{5} \delta_{BE}
$$

$$
= \frac{12}{5}(0.600 \text{ mm}) - \frac{7}{5}(0.400 \text{ mm})
$$

= 0.880 mm
(Downward)

Problem 2.2-13 A framework *ABC* consists of two rigid bars *AB* and *BC*, each having length *b* (see the first part of the figure). The bars have pin connections at *A*, *B*, and *C* and are joined by a spring of stiffness *k*. The spring is attached at the midpoints of the bars. The framework has a pin support at *A* and a roller support at *C*, and the bars are at an angle α to the hoizontal.

When a vertical load *P* is applied at joint *B* (see the second part of the figure) the roller support *C* moves to the right, the spring is stretched, and the angle of the bars decreases from α to the angle θ .

Determine the angle θ and the increase δ in the distance between points *A* and *C*. (Use the following data; $b = 8.0$ in., $k = 16$ lb/in., $\alpha = 45^{\circ}$, and $P = 10$ lb.)

Probs. 2.1-13 and 2.2-14

WITH LOAD *P* $L₂$ = span from *A* to *C* $= 2b \cos \theta$ S_2 = length of spring $=\frac{L_2}{2} = b \cos \theta$

WITH NO LOAD

 L_1 = span from *A* to *C*

 $=$ 2*b* cos α

 S_1 = length of spring

$$
=\frac{L_1}{2}=b\,\cos\,\alpha
$$

FREE-BODY DIAGRAM OF *BC*

 $h =$ height from *C* to $B = b \sin \theta$

$$
\frac{L_2}{2} = b \cos \theta
$$

 $F =$ force in spring due to load *P*

$$
\Sigma M_B = 0 \Leftrightarrow \Leftrightarrow
$$

$$
\frac{P}{2} \left(\frac{L_2}{2}\right) - F \left(\frac{h}{2}\right) = 0 \text{ or } P \cos \theta = F \sin \theta
$$
 (Eq. 1)

DETERMINE THE ANGLE θ ΔS = elongation of spring $S_2 - S_1 = b(\cos \theta - \cos \alpha)$ For the spring: $F = k(\Delta S)$ $F = bk(\cos \theta - \cos \alpha)$ Substitute *F* into Eq. (1): $P \cos \theta = bk(\cos \theta - \cos \alpha)(\sin \theta)$ or $\frac{P}{U} \cot \theta - \cos \theta + \cos \alpha = 0 \longleftarrow$ (Eq. 2) This equation must be solved numerically for the angle θ . DETERMINE THE DISTANCE δ $\delta = L_2 - L_1 = 2b \cos \theta - 2b \cos \alpha$ $= 2b(\cos \theta - \cos \alpha)$ $\frac{h}{\partial k}$ cot θ – cos θ + cos α = 0 \leftarrow From Eq. (2): $\cos \alpha = \cos \theta - \frac{P \cot \theta}{U}$ Therefore, (Eq. 3) NUMERICAL RESULTS $b = 8.0$ in. $k = 16$ lb/in. $\alpha = 45^{\circ}$ *P* = 10 lb Substitute into Eq. (2): $0.078125 \cot \theta - \cos \theta + 0.707107 = 0$ (Eq. 4) Solve Eq. (4) numerically: Substitute into Eq. (3): $\delta = 1.78$ in. \longleftarrow $\theta = 35.1^\circ \leftarrow$ $=\frac{2P}{b}$ cot $\theta \quad \leftarrow$ $\delta = 2b \left(\cos \theta - \cos \theta + \frac{P \cot \theta}{b^k} \right)$ $\frac{1}{b k}$ *bk*

Problem 2.2-14 Solve the preceding problem for the following data: $b = 200$ mm, $k = 3.2$ kN/m, $\alpha = 45^{\circ}$, and $P = 50$ N.

Solution 2.2-14 Framework with rigid bars and a spring

See the solution to the preceding problem.

EQ. (2):
$$
\frac{P}{bk} \cot \theta - \cos \theta + \cos \alpha = 0
$$

\nEQ. (3): $\delta = \frac{2P}{k} \cot \theta$

NUMERICAL RESULTS $b = 200$ mm $k = 3.2$ kN/m $\alpha = 45^{\circ}$ $P = 50$ N Substitute into Eq. (2): $0.078125 \cot \theta - \cos \theta + 0.707107 = 0$ (Eq. 4) Solve Eq. (4) numerically: Substitute into Eq. (3): δ = 44.5 mm \leftarrow $\theta = 35.1^\circ \leftarrow$

Changes in Lengths Under Nonuniform Conditions

Problem 2.3-1 Calculate the elongation of a copper bar of solid circular cross section with tapered ends when it is stretched by axial loads of magnitude 3.0 k (see figure).

The length of the end segments is 20 in. and the length of the prismatic middle segment is 50 in. Also, the diameters at cross sections *A*, *B*, *C*, and *D* are 0.5, 1.0, 1.0, and 0.5 in., respectively, and the modulus of elasticity is 18,000 ksi. (*Hint:* Use the result of Example 2-4.)

Solution 2.3-1 Bar with tapered ends

MIDDE SEGMENT
$$
(L = 50 \text{ in.})
$$

$$
\delta_2 = \frac{PL}{EA} = \frac{(3.0 \text{ k})(50 \text{ in.})}{(18,000 \text{ ksi})(\frac{\pi}{4})(1.0 \text{ in.})^2}
$$

$$
= 0.01061 \text{ in.}
$$

ELONGATION OF BAR

$$
\delta = \sum \frac{NL}{EA} = 2\delta_1 + \delta_2
$$

= 2(0.008488 in.) + (0.01061 in.)
= 0.0276 in.

Problem 2.3-2 A long, rectangular copper bar under a tensile load *P* hangs from a pin that is supported by two steel posts (see figure). The copper bar has a length of 2.0 m, a cross-sectional area of 4800 mm2, and a modulus of elasticity $E_c = 120$ GPa. Each steel post has a height of 0.5 m, a cross-sectional area of 4500 mm2, and a modulus of elasticity $E_s = 200 \text{ GPa}.$

- (a) Determine the downward displacement δ of the lower end of the copper bar due to a load $P = 180$ kN.
- (b) What is the maximum permissible load P_{max} if the displacement δ is limited to 1.0 mm?

$$
= 0.675 \text{ mm} \leftarrow
$$
\n(b) MAXIMUM LOAD $P_{\text{max}} (\delta_{\text{max}} = 1.0 \text{ mm})$ \n
$$
\frac{P_{\text{max}}}{P} = \frac{\delta_{\text{max}}}{\delta} \quad P_{\text{max}} = P\left(\frac{\delta_{\text{max}}}{\delta}\right)
$$
\n
$$
P_{\text{max}} = (180 \text{ kN}) \left(\frac{1.0 \text{ mm}}{0.675 \text{ mm}}\right) = 267 \text{ kN} \leftarrow
$$

Problem 2.3-3 A steel bar *AD* (see figure) has a cross-sectional area of 0.40 in.² and is loaded by forces $P_1 = 2700$ lb, $P_2 = 1800$ lb, and P_3 = 1300 lb. The lengths of the segments of the bar are $a = 60$ in., $b = 24$ in., and $c = 36$ in.

- (a) Assuming that the modulus of elasticity $E = 30 \times 10^6$ psi, calculate the change in length δ of the bar. Does the bar elongate or shorten?
- (b) By what amount *P* should the load P_3 be increased so that the bar does not change in length when the three loads are applied?

Solution 2.3-3 Steel bar loaded by three forces

(b) INCREASE IN P_3 for no change in length

 $P =$ increase in force P_3

The force *P* must produce a shortening equal to 0.0131 in. in order to have no change in length.

∴ 0.0131 in. =
$$
\delta = \frac{PL}{EA}
$$

= $\frac{P(120 \text{ in.})}{(30 \times 10^6 \text{ psi})(0.40 \text{ in.}^2)}$
 $P = 1310 \text{ lb}$

Problem 2.3-4 A rectangular bar of length *L* has a slot in the middle half of its length (see figure). The bar has width *b*, thickness *t*, and modulus of elasticity *E*. The slot has width *b*/4.

- (a) Obtain a formula for the elongation δ of the bar due to the axial loads *P*.
- (b) Calculate the elongation of the bar if the material is high-strength steel, the axial stress in the middle region is 160 MPa, the length is 750 mm, and the modulus of elasticity is 210 GPa.

Solution 2.3-4 Bar with a slot

 $t =$ thickness $L =$ length of bar

(a) ELONGATION OF BAR

$$
\delta = \sum \frac{N_i L_i}{EA_i} = \frac{P(L/4)}{E(bt)} + \frac{P(L/2)}{E(\frac{3}{4}bt)} + \frac{P(L/4)}{E(bt)}
$$

$$
= \frac{PL}{Ebt} \left(\frac{1}{4} + \frac{4}{6} + \frac{1}{4}\right) = \frac{7PL}{6Ebt} \longleftarrow
$$

STRESS IN MIDDLE REGION $\sigma = \frac{P}{A} = \frac{P}{\left(\frac{3}{4}bt\right)}$ $=\frac{4P}{3 \, bt}$ or $\frac{P}{bt} = \frac{3\sigma}{4}$

Substitute into the equation for δ :

$$
\delta = \frac{7PL}{6Ebt} = \frac{7L}{6E} \left(\frac{P}{bt}\right) = \frac{7L}{6E} \left(\frac{3\sigma}{4}\right)
$$

$$
= \frac{7\sigma L}{8E}
$$

(b) SUBSTITUTE NUMERICAL VALUES:

$$
\sigma = 160 \text{ MPa} \quad L = 750 \text{ mm} \quad E = 210 \text{ GPa}
$$
\n
$$
\delta = \frac{7(160 \text{ MPa})(750 \text{ mm})}{8(210 \text{ GPa})} = 0.500 \text{ mm}
$$

Problem 2.3-5 Solve the preceding problem if the axial stress in the middle region is 24,000 psi, the length is 30 in., and the modulus of elasticity is 30×10^6 psi.

Problem 2.3-6 A two-story building has steel columns *AB* in the first floor and *BC* in the second floor, as shown in the figure. The roof load P_1 equals 400 kN and the second-floor load P_2 equals 720 kN. Each column has length $L = 3.75$ m. The cross-sectional areas of the first- and secondfloor columns are 11,000 mm² and 3,900 mm², respectively.

- (a) Assuming that $E = 206$ GPa, determine the total shortening δ_{AC} of the two columns due to the combined action of the loads P_1 and P_2 .
- (b) How much additional load P_0 can be placed at the top of the column (point *C*) if the total shortening δ_{AC} is not to exceed 4.0 mm?

(a) SHORTENING δ_{AC} OF THE TWO COLUMNS

$$
\delta_{AC} = \sum \frac{N_i L_i}{E_i A_i} = \frac{N_{AB} L}{E A_{AB}} + \frac{N_{BC} L}{E A_{BC}}
$$

=
$$
\frac{(1120 \text{ kN})(3.75 \text{ m})}{(206 \text{ GPa})(11,000 \text{ mm}^2)} + \frac{(400 \text{ kN})(3.75 \text{ m})}{(206 \text{ GPa})(3,900 \text{ mm}^2)}
$$

= 1.8535 mm + 1.8671 mm = 3.7206 mm

$$
\delta_{AC} = 3.72 \text{ mm}
$$

 $P_1 = 400$ kN $P_2 = 720$ kN *B A C* $L = 3.75$ m *L* = 3.75 m (b) ADDITIONAL LOAD P_0 AT POINT C

$$
(\delta_{AC})_{\text{max}} = 4.0 \text{ mm}
$$

 δ_0 = additional shortening of the two columns due to the load P_0

$$
\delta_0 = (\delta_{AC})_{\text{max}} - \delta_{AC} = 4.0 \text{ mm} - 3.7206 \text{ mm}
$$

= 0.2794 mm

Also,
$$
\delta_0 = \frac{P_0 L}{E A_{AB}} + \frac{P_0 L}{E A_{BC}} = \frac{P_0 L}{E} \left(\frac{1}{A_{AB}} + \frac{1}{A_{BC}} \right)
$$

Problem 2.3-7 A steel bar 8.0 ft long has a circular cross section of diameter $d_1 = 0.75$ in. over one-half of its length and diameter $d_2 = 0.5$ in. over the other half (see figure). The modulus of elasticity $E = 30 \times 10^6$ psi.

- (a) How much will the bar elongate under a tensile load $P = 5000$ lb?
- (b) If the same volume of material is made into a bar of constant diameter *d* and length 8.0 ft, what will be the elongation under the same load *P*?

Solution 2.3-7 Bar in tension

$$
d_1 = 0.75
$$
 in. $d_2 = 0.50$ in.
\n $P = 5000$ lb

$$
P = 5000
$$
 lb
\n $E = 30 \times 10^6$ psi
\n $L = 4$ ft = 48 in.

(a) ELONGATION OF NONPRISMATIC BAR

$$
\delta = \sum \frac{N_i L_i}{E_i A_i} = \frac{PL}{E} \sum \frac{1}{A_i}
$$

$$
\delta = \frac{(5000 \text{ lb})(48 \text{ in.})}{30 \times 10^6 \text{ psi}}
$$

$$
\times \left[\frac{1}{\frac{\pi}{4}(0.75 \text{ in.})^2} + \frac{1}{\frac{\pi}{4}(0.50 \text{ in.})^2} \right]
$$

= 0.0589 in.

Solve for P_0 :

$$
P_0 = \frac{E\delta_0}{L} \left(\frac{A_{AB} A_{BC}}{A_{AB} + A_{BC}}\right)
$$

SUBSTITUTE NUMERICAL VALUES:

$$
E = 206 \times 10^{9} \text{ N/m}^{2} \quad \delta_0 = 0.2794 \times 10^{-3} \text{ m}
$$
\n
$$
L = 3.75 \text{ m} \quad A_{AB} = 11,000 \times 10^{-6} \text{ m}^{2}
$$
\n
$$
A_{BC} = 3,900 \times 10^{-6} \text{ m}^{2}
$$
\n
$$
P_0 = 44,200 \text{ N} = 44.2 \text{ kN} \longleftarrow
$$

(B) ELONGATION OF PRISMATIC BAR OF SAME VOLUME

Original bar: $V_a = A_1 L + A_2 L = L(A_1 + A_2)$ Prismatic bar: $V_p = A_p(2L)$ Equate volumes and solve for A_p : $V_p = V_p$ $L(A_1 + A_2) = A_p(2L)$ $\delta = \frac{P(2L)}{P}$ *EAp* $=\frac{(5000 \text{ lb})(2)(48 \text{ in.})}{(30 \times 10^6 \text{ psi})(0.3191 \text{ in.}^2)}$ $=\frac{\pi}{8}$ [(0.75 in.)² + (0.50 in.)²] = 0.3191 in.² $A_p = \frac{A_1 + A_2}{2} = \frac{1}{2}$ π $\binom{n}{4}$ $(d_1^2 + d_2^2)$

$$
= 0.0501 \text{ in.} \longleftarrow
$$

NOTE: A prismatic bar of the same volume will *always* have a smaller change in length than will a nonprismatic bar, provided the constant axial load *P*, modulus *E*, and total length *L* are the same.